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Londergan et al.

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(54) **PASSIVATION METHOD FOR IMPROVED UNIFORMITY AND REPEATABILITY FOR ATOMIC LAYER DEPOSITION AND CHEMICAL VAPOR DEPOSITION**

(58) **Field of Search** 438/680, 681, 438/785; 427/248.1, 255.39, 585

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(*) **Notice:** Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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(65) **Prior Publication Data**

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Related U.S. Application Data

(60) Provisional application No. 60/326,893, filed on Oct. 2, 2001.

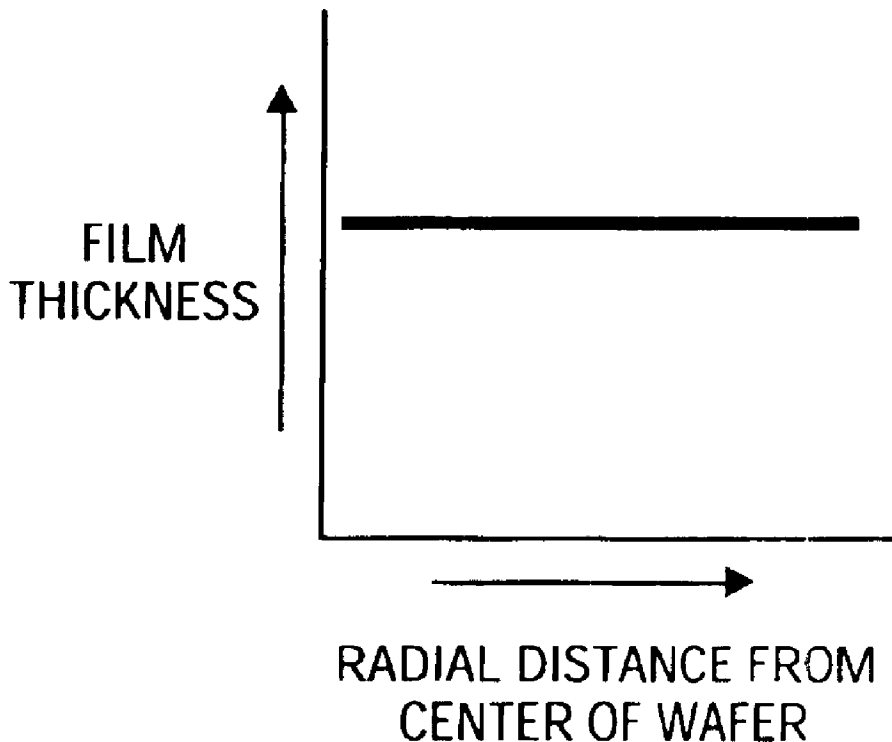
(51) **Int. Cl.⁷** **H01L 21/31**

(52) **U.S. Cl.** **438/680; 438/681; 438/785; 427/248.1**

(57) **ABSTRACT**

A method to deposit a passivating layer of a first material on an interior reactor surface of a cold or warm wall reactor, in which the first material is non-reactive with one or more precursor used to form a second materials. Subsequently when a film layer is deposited on a substrate by subjecting the substrate to the one or more precursors, in which at least one precursor has a low vapor pressure, uniformity and repeatability is improved by the passivation layer.

30 Claims, 4 Drawing Sheets



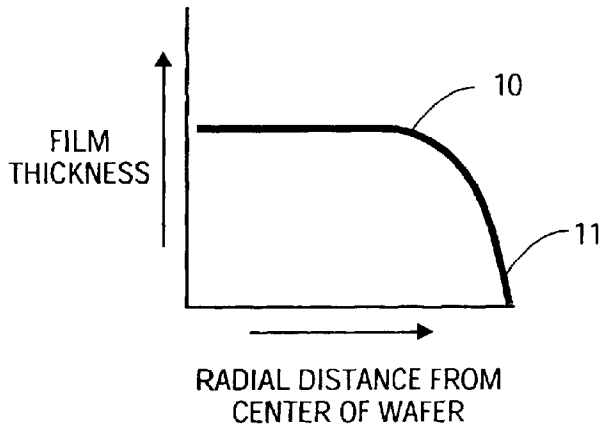


FIG. 1A
(PRIOR ART)

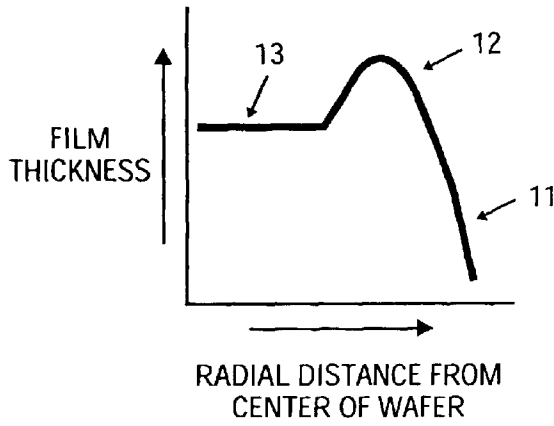


FIG. 1B
(PRIOR ART)

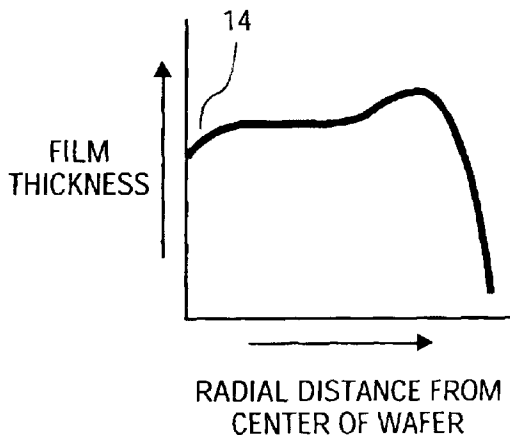


FIG. 1C
(PRIOR ART)

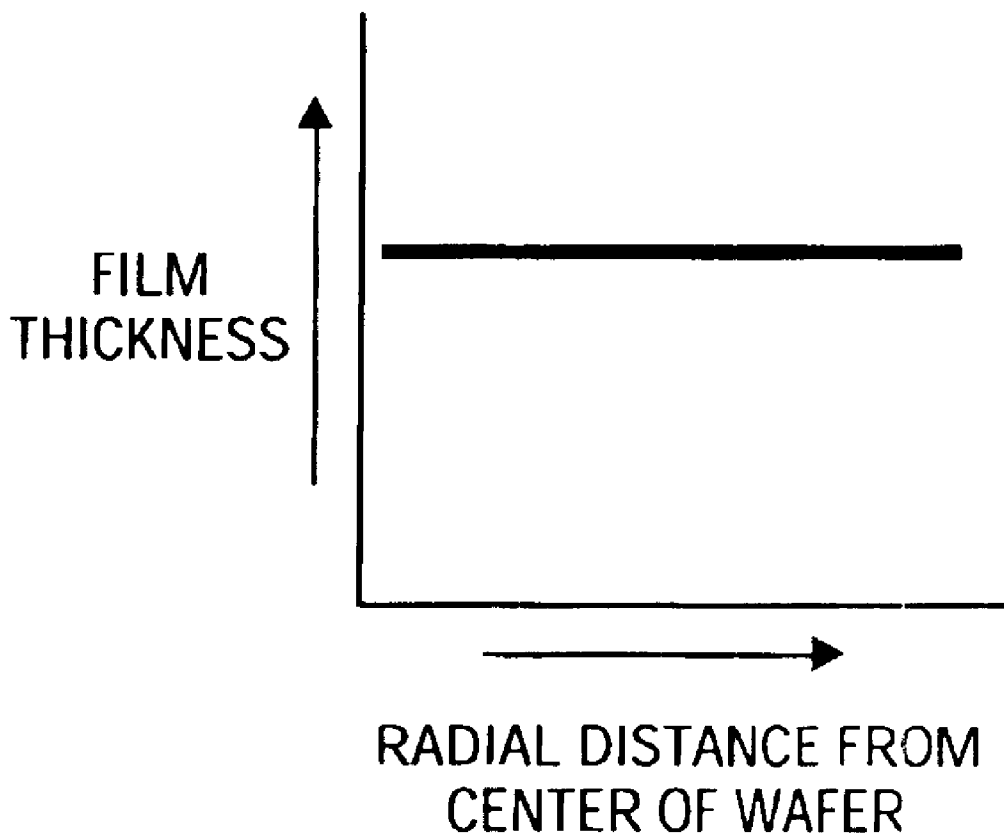


FIG. 2

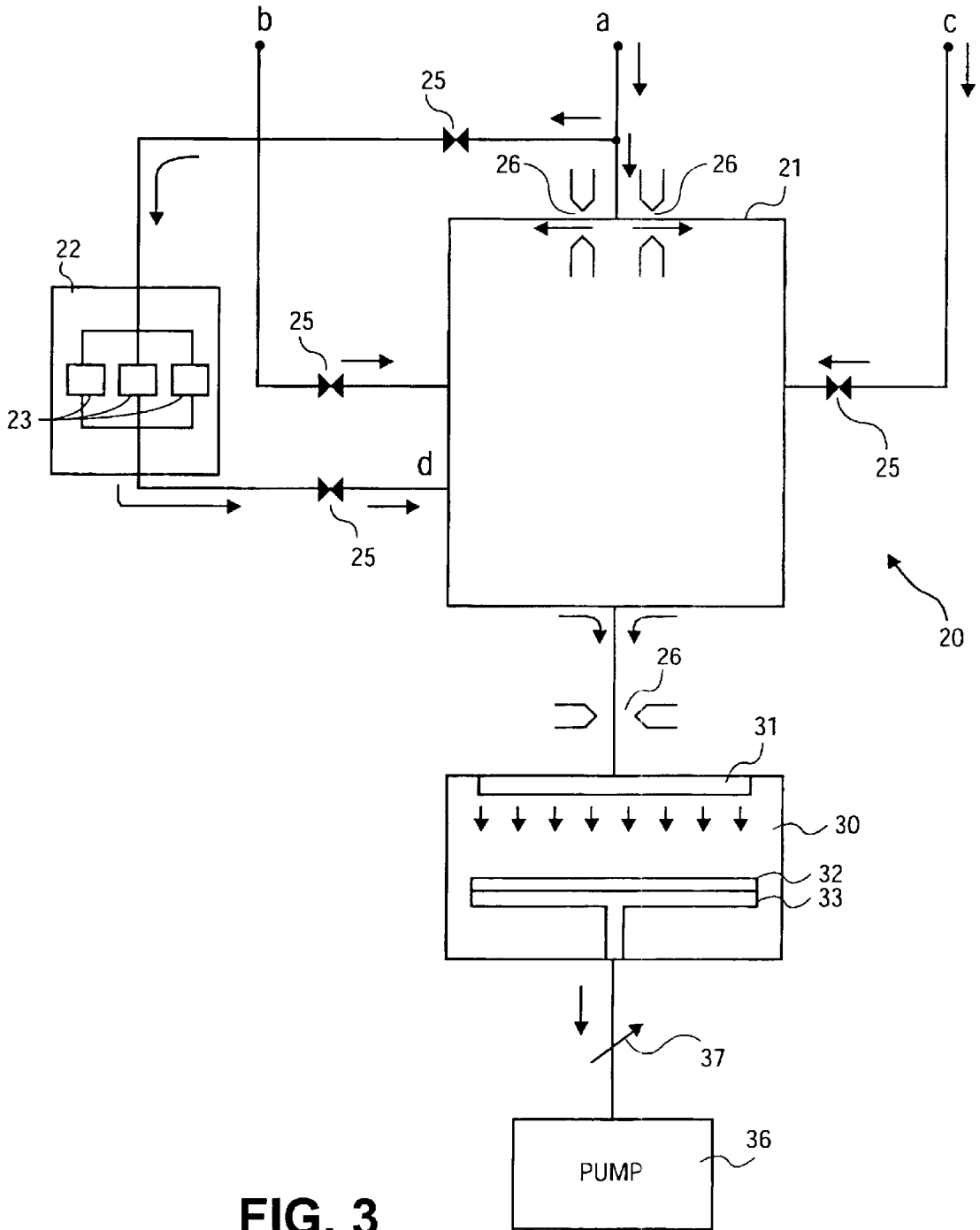


FIG. 3

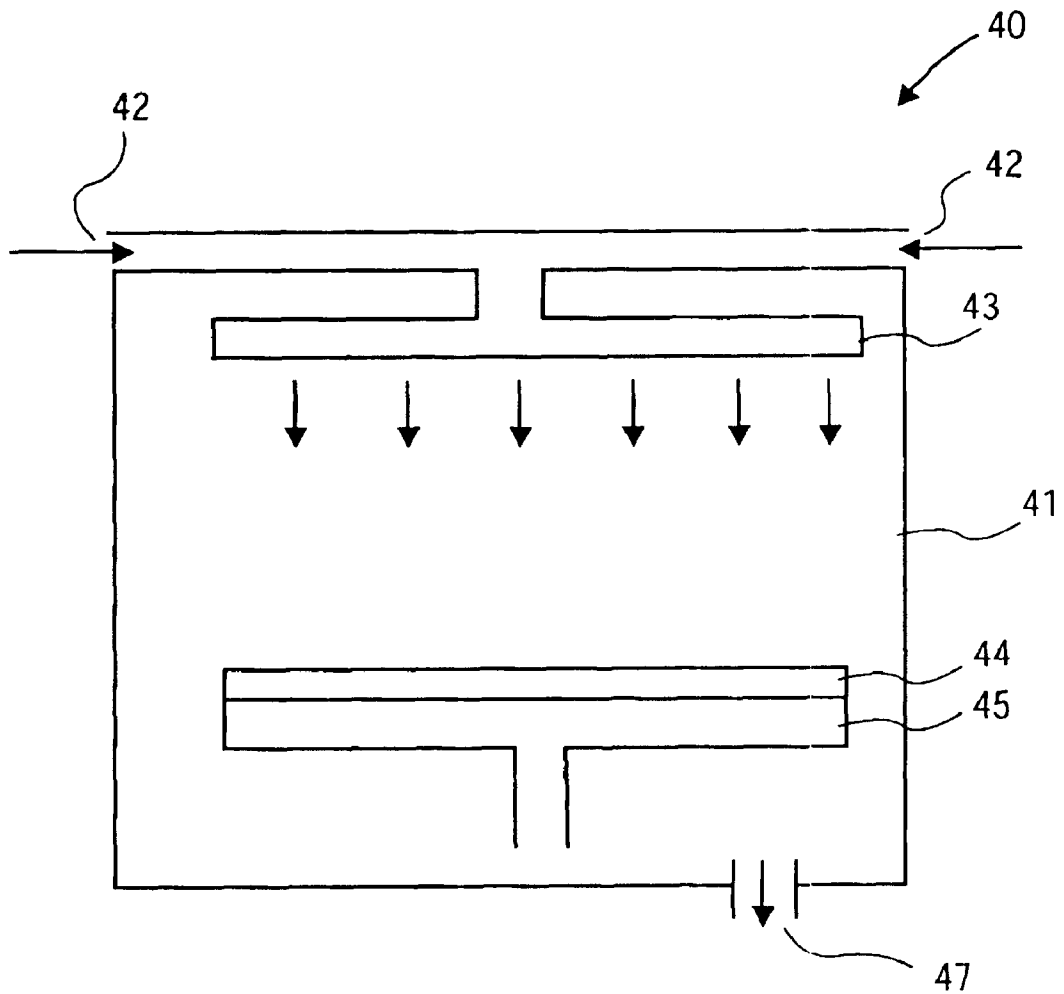


FIG. 4

**PASSIVATION METHOD FOR IMPROVED
UNIFORMITY AND REPEATABILITY FOR
ATOMIC LAYER DEPOSITION AND
CHEMICAL VAPOR DEPOSITION**

This application claims the benefit of priority from U.S. Provisional Patent Application Serial No. 60/326,893 entitled "Passivation Methods for Improved Uniformity and Repeatability for Atomic Layer Deposition" filed on Oct. 2, 2001.

FIELD OF THE INVENTION

The present invention relates to semiconductor processing and, more particularly, to a method for improved control of uniformity and repeatability in Atomic Layer Deposition and/or Chemical Vapor Deposition.

BACKGROUND OF THE RELATED ART

Chemical Vapor Deposition (CVD) is a widely used deposition process for the growth of thin films on various substrates, including semiconductor wafers. As microelectronics device dimensions are reduced, or scaled down, CVD is becoming an attractive method for the deposition of conformal films over complex device topography. Additionally, new materials are considered in the design of advanced devices. For example, high dielectric constant (k) oxide materials are attractive alternative to the conventionally employed silicon-based oxides for use as gate or capacitor dielectrics. Recently, some dynamic random access memory (DRAM) products have been manufactured, in which CVD is used to deposit high-k tantalum pentoxide (Ta_2O_5).

In the field of material deposition, a process known as Atomic Layer Deposition (ALD) has emerged as a promising candidate to extend the abilities of CVD techniques. Generally, ALD is a process wherein conventional CVD processes are divided into separate deposition steps that theoretically go to saturation at a single molecular or atomic monolayer thickness and self-terminate. For ALD applications, the molecular precursors are introduced into the reactor separately. Typically, an ALD precursor reaction is followed by inert gas purging of the reactor to remove the precursor from the reactor prior to the introduction of the next precursor.

One way of classification of the CVD/ALD type of deposition reactors is by the temperature at which the reactor wall is maintained with respect to the deposition temperature of a substrate resident in the reactor. In "cold wall" and "warm wall" reactors, the reactor chamber wall (or vacuum containing surface) is maintained at a temperature that permits physisorption or limited (or imperfect, or partial) chemisorption. This is in contrast to hot wall reactors where the wall temperature is close to or near the substrate deposition temperature, where chemisorption and deposition takes place by design.

In CVD the films are deposited from molecular precursors that are carried to the reactor in a vapor state, typically mixed with an inert carrier gas. A substrate is kept at temperature that is optimized to promote chemical reaction between the molecular precursors concurrent with efficient desorption of byproducts. Accordingly, the reaction proceeds to deposit the desired pure film. The selection of a suitable precursor is a key in CVD, as there are a number of restrictions on the precursor's physical and chemical properties. In particular, the precursor should be of sufficient volatility at temperatures below the decomposition tempera-

ture in order for the vapors to be transported to the reactor without premature decomposition. The requirement for saturation of the precursor reactions in ALD imposes additional constraints on the potential precursors.

Generally the precursors for CVD and ALD fall in 3 categories based on their volatility: 1) gases (e.g., NH_3 and WF_6); 2) high vapor pressure (e.g., 5 to 40 Torr @ room temperature (RT)) liquids (e.g., trimethyl aluminum (TMA), $SiCl_4$, $TiCl_4$, H_2O) and solids (e.g., $W(CO)_6$); and 3) low vapor pressure (e.g., less than 0.5 Torr @ RT) liquids (e.g., some metal organic Zr, Ta, and Hf precursors) and solids (e.g., $TaCl_5$, $HfCl_4$, $ZrCl_4$). Additionally some solids may be dissolved in a solvent and handled as liquids. While gases and high vapor pressure precursors are clearly desirable, such precursors are not available for the deposition of pure, high quality films by CVD or ALD.

Containers for precursors with high vapor pressure are typically maintained at room temperature and some gas lines between the precursor container and CVD or ALD reactor may be heated to a moderate temperature (e.g., $<100^\circ C.$) to reduce adsorption or condensation. In warm and/or cold (warm/cold) wall reactors, the reactor chamber walls are typically maintained at or below the temperature where precursor condensation occurs. In contrast, the containers for precursors with low vapor pressure are typically maintained at high temperature to generate sufficient vapor and gas lines between the precursor container and CVD or ALD reactor are usually heated to a temperature higher than the temperature of the precursor container to prevent condensation. When the precursor container temperature is higher than the temperature of some inner reactor surfaces, precursor condensation typically occurs on these surfaces. In CVD processes this may cause thickness non-uniformity due to precursor depletion and consequently different deposition rate on different areas on the substrate. In ALD processes some of the condensed precursor may be desorbed and travel to some areas of the substrate surface simultaneously with the second precursor, resulting in excess film thickness deposition on these areas of the substrate. The precursor that remains condensed on the reactor surfaces may react with the second precursor to form a parasitic film on these surfaces. Typically this film is of poor or inferior quality compared to the quality of the film deposited on the substrate. The net effect is depletion of one or both precursors which may result in less film thickness on some areas of the substrate due to insufficient precursor delivery to the substrate surface. Thus, various mechanisms may contribute to non-uniform film deposition and also lead to gradual deterioration of the thickness uniformity and repeatability of deposited films over time.

Thus, a need is present to improve uniformity and repeatability when depositing a film layer in ALD and CVD reactors. The need is more pronounced in depositing films on substrates using low vapor pressure precursors.

SUMMARY

A technique to deposit a passivating layer by a first chemical process on a cold or warm wall CVD or ALD reactor to improve uniformity of a film layer deposited on a substrate resident in a reactor chamber. The passivating layer is deposited as a non-reactive (inert) coating on surfaces where parasitic deposition may occur by remnants of a precursor chemical used to deposit the film layer remaining on the surfaces of the chamber. The passivating layer is non-reactive with one or more precursors used to deposit the film layer on the substrate. In one embodiment Al_2O_3 is used

as a passivation layer for deposition of film layers of high-k dielectrics, ZrO_2 and HfO_2 .

BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the present invention are illustrated by way of example and are not for the purpose of limitation. In the figures of the accompanying drawings, similar references are utilized to indicate similar elements.

FIG. 1A is a graphic illustration of a prior art deposition process in which the deposition thickness of the film layer decreases at the periphery of the wafer.

FIG. 1B is a graphic illustration of a prior art deposition process in which the deposition thickness of the film layer increases slightly before decreasing at the periphery of the wafer.

FIG. 1C is a graphic illustration of a prior art deposition process in which the deposition thickness of the film layer decreases at the center of the wafer, as well as at the periphery of the wafer.

FIG. 2 is a graphic illustration of a deposition process in which a passivating layer applied to the interior of the reactor chamber improves the uniformity of the thickness of the film layer deposited.

FIG. 3 is one representative example of an ALD reactor system to utilize the passivation technique of the present invention.

FIG. 4 is one representative example of a CVD reactor system to utilize the passivation technique of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

In the description below, the present invention is described in reference to various embodiments. In order to understand the invention, particular examples are given. The example embodiments describe the deposition of ZrO_2 and HfO_2 and processes related to depositing ZrO_2 and HfO_2 film layers on a substrate. Furthermore, the processes described pertain to ALD and CVD. However, the invention is not limited to these processes or chemistries. Thus, other materials, including films other than high-k materials, may be readily deposited utilizing the passivation techniques of the present invention. Additionally, the invention is more applicable with cold and/or warm (cold/warm) wall reactors, which are defined as a vacuum containing surface that is maintained at a temperature that permits physisorption or limited or imperfect or partial chemisorption. This is in contrast to hot wall reactor whose wall temperature is close to or near the substrate temperature, where chemisorption and film deposition takes place by design.

In the deposition of ZrO_2 and HfO_2 , one of the more common inorganic metal precursors used to deposit ZrO_2 and HfO_2 are $ZrCl_4$ and $HfCl_4$, respectively. Both materials are solids with low vapor pressure. Therefore, they are typically heated to a temperature in the approximate range of 155–180° C. in order to generate sufficient vapor for film deposition. The vapors are carried to an ALD reactor with the use of an inert carrier gas, such as Ar, He or N_2 . For ALD, ZrO_2 films are grown by alternating $ZrCl_4$ and H_2O pulses, in the fashion typically employed with known ALD reactors. Similarly, ALD HfO_2 films are grown by alternating $HfCl_4$ and H_2O precursor pulses in an ALD reactor.

Keeping with ALD processes, process parameters, such as deposition temperature and pressure, precursor doses, and purge times are generally optimized to yield highly uniform

films with precisely controlled thickness. However, unlike other ALD processes, the uniformity of some films (such as ALD deposited ZrO_2 films) is observed to deteriorate with increasing number of processed wafers and/or accumulated film thickness. The following examples generally illustrate trends in ALD of ZrO_2 performed in a vertical flow warm wall ALD reactor, where the temperature of inner reactor surfaces, such as wall is in the range of 100 to 140° C. This temperature is substantially lower than the temperature of the $ZrCl_4$ container, which is in the range of 170–180° C. FIG. 1 (namely, FIGS. 1A, 1B and 1C) show representative examples of degradation trends in the thickness uniformity profile.

A first example illustration in FIG. 1A shows a graphic comparison of deposited film thickness over a radial profile of the wafer from its center to the periphery. As noted, the thickness profile of the deposited film is fairly uniform except near the periphery of the substrate (such as a semiconductor wafer). In reference to ZrO_2 , as the total deposited ZrO_2 film thickness exceeds a certain thickness (usually greater than 50 Å, and more typically at around 300 Å), the uniformity starts to deteriorate at about location 10, and the film thickness is less towards the edge of the wafer, as shown at location 11. A variety of causes may contribute to the thickness deterioration at the periphery, but generally, it is due to insufficient saturation of the wafer surface by the precursor at the periphery. For example, the deterioration of uniformity of the deposited film may be attributed to depletion of at least the halide due to condensation on the interior surfaces of the warm wall reactor. That is, remnants of one precursor on the walls of the reactor chamber may cause parasitic deposition on the reactor wall with the introduction of the subsequent precursor. Accordingly, deposition occurs on the interior surfaces of the reactor that may be of inferior quality and thus may further deplete the precursor available for deposition on the wafer surface due to enhanced adsorption.

In a second example shown in FIG. 1B, the example illustrates a thickness profile of approximately 70 Å ZrO_2 film after approximately 1000 Å total ZrO_2 thickness has been deposited on previous wafers. Again, there is very little or no deposition towards the wafer edge at location 11. Furthermore, another feature characteristic of this profile is an area 12 with increased thickness, located between the relatively uniform deposition in the center region 13 and the edge location 11 of the wafer. This region of increased thickness is found to be generally independent of the processing conditions. The increased thickness of area 12 is likely due to parasitic deposition on the wafer occurring in parallel with the ALD reaction. Again the thinner deposition at the wafer edge is presumably due to a result of starved reaction, where one or both precursors are not present in sufficient quantity to reach saturation. The mechanism is likely related to the chemistry used in the particular ALD process, namely $ZrCl_4$ and H_2O . However, it may also be observed in the reaction of the precursor, $ZrCl_4$, with one of a variety of non-metallic reactants (oxidizing and nitriding agents).

FIG. 1C illustrates a situation in which non-uniformity is noted at the center region 14 of the wafer, as well as at the periphery 11. It is possible that in some instances, parasitic deposition region 12 may also be appreciable. The decrease in the deposition thickness at the center of the wafer may be attributed in some instances to the presence of a distributor plate or “shower head” with blocked center area. Distributor plates and shower heads generally used in ALD and CVD reactors to distribute or disperse the gas at the inlet, so as to

have even gas flow across the wafer surface. However, in comparison to the side walls of the reactor, the distribution structure(s) (e.g., distributor plate, shower head, etc.) may contribute more strongly to depletion of at least one of the precursors, H₂O or a halide due to condensation, adsorption and parasitic deposition on the structure. This is because distribution structure(s) are typically located in the path of the precursor flow. As a result, generally, faster deterioration of film thickness uniformity may be observed in systems equipped with a distribution structure.

Furthermore, the non-uniform deposition thickness profile may manifest itself across a single processed wafer profile (thickness non-uniformity) or it may manifest the non-uniformness over repeated wafers (non repeatability). That is, although the first (or first set) of wafer depositions may be somewhat uniform, wafers processed subsequently may exhibit the deteriorating profile(s).

The profiles illustrated in FIGS. 1A, 1B and 1C are axi-symmetric and consistent with gas injection in vertical ALD reactor systems. The profile trend signature from an ALD reactor with horizontal flow may be different (consistent with unidirectional flow above the wafer), but uniformity problems may be present, similar to the vertical reactor systems.

In regards to the deposition of HfO₂, similar uniformity problems of ALD HfO₂ films may occur, but at a slower rate. This is because the HfCl₄ container is typically heated to a lower temperature in comparison with the ZrCl₄ container. Accordingly, precursor condensation on interior reactor surfaces is less pronounced. For example, it may take 500 to 1000 Å of total ALD HfO₂ film thickness to observe the change in uniformity at the periphery of the wafer.

The practice of the present invention establishes that certain passivation processes of the ALD/CVD reactor provide improved uniformity and repeatability of the ALD/CVD deposition process. In one particular embodiment for ALD processes, such passivation may be practiced by performing a short Al₂O₃ deposition on the interior of an ALD reactor chamber. In one embodiment, Al₂O₃ deposition may be practiced using an ALD sequence. For example, Al₂O₃ may be deposited using an organic Al precursor and an oxidizer. In one particular embodiment Tri-Methyl Aluminum (TMA) and H₂O may be used as ALD precursors to deposit Al₂O₃. The passivation may be applied to coat the walls of the reactor and/or to coat exposed structures, such as distributor plates and shower heads

The passivation deposition results in a deposition of a non-reactive layer (coating), which reduces adsorption of precursors and/or coat over remnant reactants from earlier introduction of precursor(s). Therefore, the passivation coating inhibits undesired reactions, which may detract from obtaining saturation of the precursor at the wafer surface. Furthermore, the passivation coating also inhibits the ability for parasitic deposition to occur, since parasitic reactions are reduced. With the deposition of the passivation layer as a coating on the reactor wall, as well as reactor components where previous precursor material may collect, improved uniformity is achieved, as shown in a substantially flat deposition profile of FIG. 2.

In one particular embodiment, a rapid switching ALD reactor system is employed to rapidly switch between deposition of ZrO₂ and Al₂O₃. In this respect, ZrO₂ film is deposited by ALD on the surface of a wafer. Prior to introducing a wafer into the reactor chamber, the reactor sidewall (as well as other structures in-line to the gas flow) is subjected to an Al₂O₃ deposition to condition the chamber.

After the Al₂O₃ deposition is completed, the wafer is transported into the reactor to undergo the ZrO₂ deposition. Then, the wafer is removed and followed by another Al₂O₃ conditioning, prior to the next wafer for depositing ZrO₂.

The length of the Al₂O₃ conditioning process is optimized to give most stable performance for the particular ALD system and desired ZrO₂ film thickness, while satisfying the requirements for high throughput. For example, when Al₂O₃ is deposited by TMA and water, as little as 30 cycles of TMA and water (approximately 20 Å of Al₂O₃) may be sufficient to ensure repeatability in the deposition of ~100 Å ZrO₂ films. However, increasing the number of conditioning cycles to approximately 60, may allow formation of thicker, continuous Al₂O₃ layer and, thus, complete passivation of the ALD system, resulting in excellent process repeatability at the expense of only slightly lower throughput time. Again, the consistent thickness uniformity profile with the use of system passivation with Al₂O₃ is illustrated in FIG. 2.

It is to be noted that the passivation coating need not be performed after each wafer. Rather, depending on the desired ZrO₂ film thickness and the desired within wafer thickness uniformity specification, the above described sequence may be modified to perform chamber conditioning after a given number of ZrO₂ wafers is processed. For example, the procedure may be optimized to allow five to ten ZrO₂ films thinner than approximately 50 Å to be deposited between every chamber conditioning. In this example, wafer to wafer thickness repeatability specifications may be more relaxed. Thus, the passivation coating may be applied after a given number of wafers. Alternatively, ZrO₂ films thicker than approximately 500 Å may require chamber conditioning after every wafer. Various sequences of passivation and deposition may be practiced.

In a processing sequence where more than one wafers are processed in between chamber conditioning steps, there may be a first wafer effect. This refers to a trend in the deposition results, where the film characteristics on the first wafer, such as film thickness, growth rate or uniformity, may be different from the film characteristics on the remaining wafers in the set due to different wall conditions for the first wafer deposition. Specifically, the ZrO₂ film may exhibit lower growth rate on the first wafer. One approach to solve this difference is to add a small number of ZrCl₄ cycles, alternating with H₂O cycles, at the end of the Al₂O₃ passivation recipe. The number of cycles may be optimized to satisfy a trade-off between throughput and uniformity specifications. For example, as little as five ZrCl₄ alternating with H₂O cycles may be sufficient to prevent first wafer effect in a given ALD system. Increasing the number of these cycles may improve repeatability, but would also lower the throughput and shorten the time between chamber conditioning steps.

It is to be noted that the procedures described above may also be applied to ALD or CVD of oxide materials following a deposition reaction mechanism of the type: ML_x+AH_z→MA_y+HL, where M is a metal; A is a non-metal; x, y and z are numbers; and ML_x is a metal halide precursor, including but not limited to one, where M is one of: Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Sr, La and L is one of F, Cl, Br, I. Another example of low vapor pressure metal precursors are some metal nitrates M(NO₃)_x, where M designates a metal atom and x is an integer.

It is to be noted that various combinations may be used to deposit the film layer following passivation, including the depositions of: metal oxide using respective metal chloride

and H₂O; metal oxide using respective metal halide and H₂O; metal oxide using metal halide and an oxidizer; metal oxide using a low vapor pressure metal precursor and an oxidizer; alloy or nanolaminate film structure having at least a first sub-layer deposited using a low vapor pressure precursor, alloy or nanolaminate film structure having at least a first material deposited using a high vapor pressure precursor; and nitride equivalents thereof. Accordingly, a metal precursor with high vapor pressure or a gas may be combined with a nitriding or oxidizing agent. Examples of oxidizing agents include H₂O, H₂O₂, O₂, O₃ and alcohol (R—OH, where R designates an alkyl group). Examples of nitriding agents include NH₃, N₂H₄ and N₂. These are example only and are not for the purpose of limiting the invention.

For example, all procedures described above may be applied to ALD of HfO₂, in which HfCl₄ and H₂O are used to deposit HfO₂. The uniformity of ALD HfO₂ films generally changes in a way similar to the ZrO₂, however at a slower rate. For example, it may take 500 to 1000 Å of ALD HfO₂ film thickness to observe the change in uniformity. Similar to the ALD of ZrO₂, the ALD HfO₂ film uniformity recovers after chamber conditioning by the passivation coating. With respect to this difference, a procedure where the chamber conditioning is carried out after a given number of wafers, such as every five to twenty-five wafers (or deposition cycles), may be more applicable for ALD of HfO₂.

Alloying the ZrO₂ and HfO₂ with Al₂O₃ to form the respective aluminates improves the repeatability, as chamber passivation occurs simultaneously with the ALD deposition during the Al₂O₃ part of the deposition sequence. Similarly, the deposition of ZrO₂/Al₂O₃ or HfO₂/Al₂O₃ nanolaminate structures also provides good process stability. Thus, in the processing of alloy or nanolaminate films the ALD system passivation may be used, but with less frequency of passivation coating.

Other methods for system passivation may involve plasma treatment. Plasma could be established in the ALD or CVD reactor and system during exposure of non-metal precursors (—AH_x, such as H₂O, H₂O₂ or alcohol (R—OH, where R designates an alkyl group)), as well as gasses such as H₂ and O₂). Generally, the passivation layer can be deposited using most any CVD or ALD based process.

Furthermore, when nitride based film deposition (Ta_nN_x, Zr_nN_x, Hf_nN_x, etc., where x is a number) from the respective low vapor pressure precursors are desired, instead of Al₂O₃, AlN_x (where x is a number) may be deposited as the passivation coating. AlN_x may be deposited from a metal organic Al precursor and a nitriding agent, such as NH₃, N₂H₄ or N₂. AlN_x may be deposited using thermal ALD or CVD or using plasma based process. Other examples of passivation materials include, but are not limited to SiO₂, Si_nN_x and BN_x, deposited using high vapor pressure precursors or gasses.

The described reactor chamber passivation technique reacts and/or coats surfaces inside the ALD reactor to restore the chamber to a desirable state for reproducible ALD deposition employing the various described chemistries. The mechanism for improved reproducibility may include, but is not limited to passivation of conduits, valves, reactor surfaces leading to the reaction surface of the wafer upon which the ZrO₂, HfO₂, or other material is deposited.

Furthermore, it is to be noted that generally, the lower the vapor pressure of the precursor, the more frequently the passivation precoat is to be carried out. For example, Ta₂O₅

may require it very infrequently, HfO₂ may require precoat somewhat frequently, and ZrO₂ may require it frequently (as often as after every wafer). This is due to the decrease in the vapor pressure from TaCl₅ through HfCl₄ to ZrCl₄. For example, in order to generate approximately 1 Torr of vapor pressure the TaCl₅, HfCl₄ and ZrCl₄ precursor material has to be heated to about 120, 180, and 190° C., respectively. Generally, as the vapor pressure of the metal precursor decreases, more frequent need for the passivation coating due to increased tendency for condensation. Typically, for the passivation layer/coating, it is deposited from high vapor pressure precursors and is non-reactive with respect to the precursors used to deposit the desired film. Additionally, the passivation coating need not be performed with the same process as the one used to deposit the film on the wafer. The growth rate (and consequently the throughput) may be increased by, for example, shortening the pulse and/or purge times compared to the ones used in a standard ALD deposition. Furthermore, other oxide films of interest may also include very high-k materials and ferroelectric films, such as barium strontium titanate (BST), lead zirconium titanate (PZT), etc. In addition to conventional semiconductor applications, the passivation techniques described may be adapted for use for optoelectronics applications, flat panel displays, superconducting oxide films, as well as others.

It is to be noted that the embodiments described above may be performed in a variety of reactor chambers utilized for deposition of film layers. However, as noted, the described techniques for passivation are generally practiced with cold/warm wall reactors employing ALD or CVD processes. Thus, one example ALD system is illustrated in FIG. 3 and an example CVD system is illustrated in FIG. 4.

Referring to FIG. 3, it shows one embodiment of an ALD system 20, having a switching manifold 21. The switching manifold 21 is coupled to a chemical source array 22, which may contain one or more chemical source(s) 23. Low vapor pressure precursor chemicals are typically contained within the source array 22.

In FIG. 3, an inert gas (such as nitrogen or argon) enters the manifold 21 at inlet "a" and is routed through a by-pass to the source array 22. The main flow is to the manifold 21, which has a split flow design to have more than one path for the gas flow. In the example diagram, two flow paths are shown in the manifold 21. Inlet "b" is coupled to one path, while inlet "c" is coupled to the other path. Various chemicals are introduced through inlets "b" and "c". In one embodiment, non-metals are introduced through inlet "c", while metal chemicals are introduced through inlet "b", both at ordinary vapor pressure. The low vapor pressure source(s) is/are introduced to the manifold 21 through inlet "d". As noted valves 25 and the passing through a port 26 control and/or regulate the flow.

The split flow of carrier gas is introduced into a reactor chamber 30 of a processing reactor. The separate flow may be kept separate to enter the chamber 30 or, alternatively as shown, the split flow may be recombined at the manifold prior to being introduced into the chamber 30 through port 26. The chamber 30 may include a distributor plate (or shower head) 31. The substrate 32 or other workpiece receiving the deposition resides in the chamber 30, typically atop a chuck (or support) 33. Downstream, a pump 36 may be present to provide low or vacuum pressure to sustain the gas flow. A throttle valve 37 may be present to regulate the flow.

Accordingly, with the ALD system 20, low vapor pressure precursors for ALD deposition of the film layer on the

substrate is provided by the source 23 and introduced into the manifold 21 at inlet "d". The passivation chemistry may be introduced through inlets "b", "c" and/or "d", depending on the chemistry. In the example of having TMA and H₂O deposit Al₂O₃ by ALD, the TMA is introduced through inlet "b" and H₂O is introduced through inlet "c". Thus, ALD system may employ ALD processes to deposit the passivation material. In other embodiments, the passivation layer may be obtained without ALD, but the film layer deposited on the substrate may still employ ALD or CVD.

One advantage of an ALD system, such as the ALD system of FIG. 3, is the ability to deposit just a few monolayers of the passivation material, as well as the film layer deposited on the substrate. The ability to control the molecular monolayer allows tight tolerances and control of the deposition process. When the passivation coating is deposited by ALD, the deposition thickness may be controlled to few (approximately 1 to 10) monolayers or many more monolayers.

A CVD system 40 having a reactor chamber 41 is shown in FIG. 4. In a typical CVD reactor, the precursors are applied together, instead of in separate stages. One or more inlets 42 introduce the precursors, which are usually distributed and dispersed through a distribution plate or a shower head 43. A substrate (or workpiece) 44 resides atop a chuck or support 45. A CVD process then results in the deposition of the film layer when precursor chemicals are introduced into the chamber 41. Spent gases are exhausted through opening 47.

As with the ALD system of FIG. 3, the CVD system may also introduce the passivating chemistry through one or more of the inlets to the chamber 42. In both systems, the passivating chemistry will coat the interior of the chamber walls, and other structures, which come in contact. The practice of depositing the passivating layer may be practiced in a variety of other reactor designs and are not limited to the two examples shown in FIGS. 3 and 4.

Thus, passivation method for improved uniformity and repeatability for atomic layer deposition and chemical vapor deposition is described. Although the passivating layer is more applicable to cold wall or warm wall ALD and/or CVD reactors, the passivation technique is not limited to such reactor types.

We claim:

1. A method comprising:

depositing a passivating layer of a first material on an interior reactor surface of a cold or warm wall reactor, in which the first material is non-reactive with one or more precursors used to form a second material; and depositing a film layer of the second material on a substrate by subjecting the substrate to the one or more precursors, in which at least one precursor has a low vapor pressure.

2. The method of claim 1 wherein said depositing of the passivating layer and the film layer are performed in an ALD or CVD reactor.

3. The method of claim 1, wherein said depositing of the passivating layer is performed by ALD or CVD technique.

4. The method of claim 2, wherein said depositing the passivating layer deposits Al₂O₃.

5. The method of claim 4, wherein depositing Al₂O₃ forms Al₂O₃ from Tri Methyl Aluminum (TMA) and H₂O.

6. The method of claim 4, wherein depositing Al₂O₃ forms Al₂O₃ from a metal organic Al precursor and an oxidizer.

7. The method of claim 2, wherein said depositing the passivating layer deposits AlN_x, where x is an number, from a metal organic Al precursor and a nitriding agent.

8. The method of claim 2, wherein said depositing the passivating layer deposits the passivating layer from a gas or high vapor pressure metal precursor and a nitriding or oxidizing agent.

9. The method of claim 2, wherein the second material is ZrO₂ deposited on the substrate using ZrCl₄ and H₂O.

10. The method of claim 2, wherein the second material is a metal oxide deposited on the substrate using the respective metal chloride and H₂O.

11. The method of claim 2, wherein the second material is a metal oxide deposited on the substrate using the respective metal halide and H₂O.

12. The method of claim 2, wherein the second material is a metal oxide formed from a group consisting of an oxide of Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Pb, La and Sr, deposited on the substrate using a respective metal halide and H₂O.

13. The method of claim 2, wherein the second material is a metal oxide formed from a group consisting of an oxide of Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Pb, La and Sr, deposited on the substrate using a respective metal halide and an oxidizer.

14. The method of claim 2, wherein the second material is a metal oxide formed from a group consisting of an oxide of Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Pb, La and Sr, deposited on the substrate using a respective low vapor pressure metal precursor and an oxidizing or nitriding agent.

15. The method of claim 2, wherein the second material is an alloy or nanolaminate film structure including at least a first component or sub-layer deposited using a low vapor pressure precursor.

16. A method comprising:

depositing a passivating layer of a first material on an interior reactor surface of a cold or warm wall reactor, in which the first material is non-reactive with one or more precursors used to form a second material; and

depositing a film layer of the second material on a substrate by subjecting the substrate to the one or more precursors, in which at least one precursor has a low vapor pressure; the passivating layer to improve uniformity and repeatability of the second material.

17. The method of claim 16 wherein said depositing of the passivating layer and the film layer are performed in an ALD or CVD reactor.

18. The method of claim 16 wherein said depositing of the passivating layer is performed by ALD or CVD technique.

19. The method of claim 17, wherein said depositing the passivating layer deposits Al₂O₃.

20. The method of claim 19, wherein depositing Al₂O₃ forms Al₂O₃ from Tri Methyl Aluminum (TMA) and H₂O.

21. The method of claim 19, wherein depositing Al₂O₃ forms Al₂O₃ from a metal organic Al precursor and an oxidizer.

22. The method of claim 17, wherein said depositing the passivating layer deposits AlN_x, where x is an number, from a metal organic Al precursor and a nitriding agent.

23. The method of claim 17, wherein said depositing the passivating layer deposits the passivating layer from a gas or high vapor pressure metal precursor and a nitriding or oxidizing agent.

24. The method of claim 17, wherein the second material is ZrO₂ deposited on the substrate using ZrCl₄ and H₂O.

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25. The method of claim 17, wherein the second material is a metal oxide deposited on the substrate using the respective metal chloride and H₂O.

26. The method of claim 17, wherein the second material is a metal oxide deposited on the substrate using the respective metal halide and H₂O. 5

27. The method of claim 17, wherein the second material is a metal oxide formed from a group consisting of an oxide of Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Pb, La and Sr, deposited on the substrate using a respective metal halide and H₂O. 10

28. The method of claim 17, wherein the second material is a metal oxide formed from a group consisting of an oxide of Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Pb, La and Sr,

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deposited on the substrate using a respective metal halide and an oxidizer.

29. The method of claim 17, wherein the second material is a metal oxide formed from a group consisting of an oxide of Zr, Hf, Ti, Ta, Al, Si, W, Zn, Mg, Ba, Bi, Pb, La and Sr, deposited on the substrate using a respective low vapor pressure metal precursor and an oxidizing or nitriding agent.

30. The method of claim 17, wherein the second material is an alloy or nanolaminate film structure including at least a first component or sub-layer deposited using a low vapor pressure precursor.

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